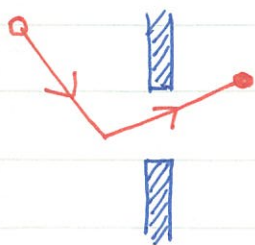
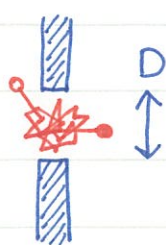


## HH0047 Law of Rarefied Gases

Once we realize the existence of mean free path  $\ell$ , the transport is separated into two regimes: effusion and diffusion. To



$$\lambda \gg D$$



$$\lambda \ll D$$

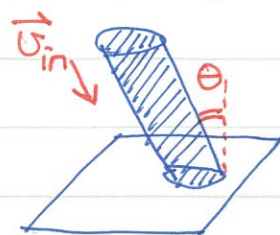
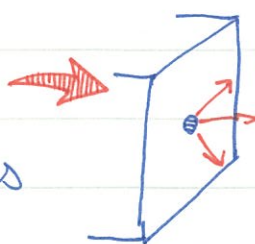
describe molecular effusion, we just need to "count" the particles without collisions. On the other hand, diffusion is naturally described by hydrodynamic approach ☺

effusion. diffusion. Let's work out several examples to understand effusion better ☺

### ① Effusion through a hole.

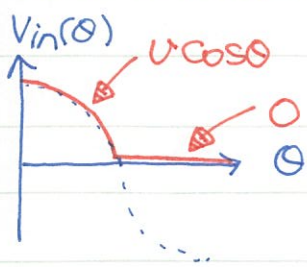
The Maxwell distribution tells us

$$\int_0^\infty dv \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin\theta \cdot \frac{1}{4\pi} P_M(v) = 1$$



The flux density of particles can be computed by averaging over the solid angle,

$$J_n = n \int_0^\infty dv \int_0^{2\pi} d\phi \int_0^1 d(\cos\theta) v_{in} \frac{1}{4\pi} P_M(v)$$



$$\rightarrow J_n = n \cdot \left[ \frac{1}{4\pi} \int_0^{2\pi} d\phi \int_0^1 d(\cos\theta) \cdot \cos\theta \right] \rightarrow \frac{1}{4} \times \left[ \int_0^\infty dv \cdot v P_M(v) \right] \rightarrow \bar{c}$$

Thus, we obtain

$$J_n = \frac{1}{4} n \bar{c}$$

Meanwhile, we can find the velocity dist through the hole:

$$P(v) dv = \frac{\frac{1}{4} n \cdot v P_M(v) \cdot dv}{\frac{1}{4} n \int_0^\infty dv v P_M(v)} = \frac{v}{\bar{c}} P_M(v) dv$$

Therefore, velocity dist. for effusion through a hole is

$$P(v) = \frac{v}{\bar{c}} P_M(v) \propto v^3 e^{-Mv^2/2\tau}$$

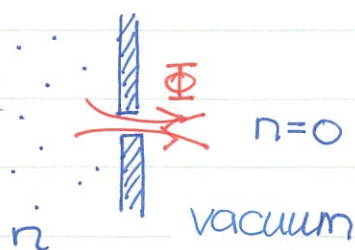
as taught in previous lecture.

When two types of gas molecules are present, the flux ratio at constant temperature is

$$\frac{J_1}{J_2} = \frac{n_1 \bar{c}_1}{n_2 \bar{c}_2} = \frac{n_1}{n_2} \sqrt{\frac{M_2}{M_1}}$$

Graham's law

It's quite useful to separate isotopes ☺



Following the "Ohm's law", we can define the conductance of the hole.

$$\Delta V = IR \rightarrow I = \frac{\Delta V}{R} = \underline{G} \cdot \Delta V$$

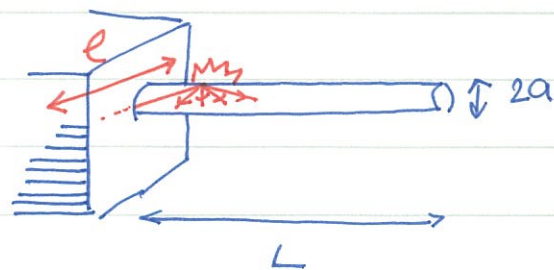
↑ conductance.

Similarly, driving the particle flux

$\Phi = J_n \cdot A$  is the difference in densities  $\Delta n = n - 0 = n$ ,

$$\rightarrow \Phi = J_n A = \left(\frac{1}{4} \bar{c} A\right) n \equiv \underline{S} \Delta n, \text{ i.e. } \underline{S} = \frac{1}{4} \bar{c} A$$

① Effusion through a tube. Consider the regime  $a \ll l \ll L$  and the reflection on the surface inside the tube is diffuse. The striking rate at the surface is  $J_n \cdot A$ . Thus, the momentum transfer rate is



$$M \langle u \rangle \cdot J_n \cdot A = \Delta P \cdot \pi a^2 \quad \leftarrow J_n = \frac{1}{4} n \bar{c} \ \& \ A = 2\pi a L$$

Solve for the drift velocity  $\langle u \rangle = \frac{\Delta P}{n M \bar{c}} \frac{2a}{L} \propto \Delta P$

The particle flux through the tube,

$$\Phi = n \cdot \langle u \rangle \cdot \pi a^2 = \left(\frac{2\pi a^3 \tau}{M \bar{c} L}\right) \frac{\Delta P}{\tau} = \left(\frac{2\pi a^3 \tau}{M \bar{c} L}\right) \cdot \Delta n$$

According to the definition of conductance  $\Phi = S \cdot \Delta n$

$$\underline{S}_{\text{tube}} = \frac{2\pi a^3 \tau}{M \bar{c} L}$$

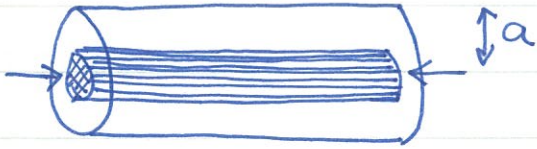
Note that  $\bar{c}^2 = 8\tau/\pi M$ , the conductance can be rewritten in more familiar form,

$$S_{\text{tube}} = \left(\frac{1}{4} \bar{c} \cdot \pi a^2\right) \cdot \frac{\pi a}{L}$$

$\underline{S}_{\text{hole}}$

$$\frac{S_{\text{tube}}}{S_{\text{hole}}} = \frac{\pi a}{L} \ll 1$$

① Diffusion through a tube: Now consider transport in hydrodynamic regime, the momentum transfer is due to viscosity. Consider a cylindrical part of radius  $r < a$ .



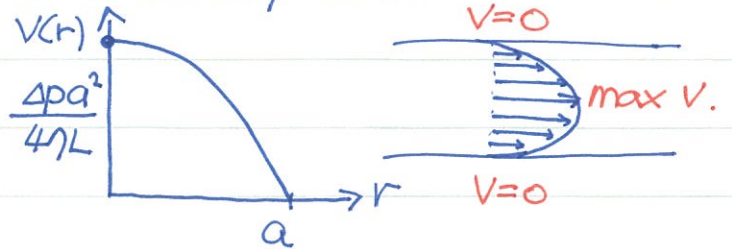
Note that the velocity  $v(r)$  vanishes on the surface  $r=a$ .

The rate of momentum transfer is balanced:

$$\Delta p \cdot \pi r^2 = (-\eta \cdot \frac{dv}{dr}) \cdot 2\pi r L \rightarrow \frac{dv}{dr} = - \frac{\Delta p}{2\eta L} \cdot r$$

It is straightforward to find the velocity  $v(r)$ .

$$v(r) = \frac{\Delta p}{4\eta L} (a^2 - r^2)$$



Integrate over  $r$  to find the particle flux:

$$\Phi = n \int_0^a v(r) \cdot 2\pi r dr = \frac{n \cdot \Delta p}{4\eta L} \cdot 2\pi \int_0^a (a^2 - r^2) r dr \quad \frac{1}{4} a^4$$

$$= \frac{n\pi a^4}{8\eta L} \cdot \Delta p$$

Express the viscosity coefficient  $\eta = \frac{1}{3} n m \bar{c} \ell$  to simplify the result.

$$\rightarrow \Phi = \left( \frac{3\pi a^4 \tau}{8M\bar{c}\ell L} \right) \cdot \frac{\Delta p}{\tau}$$

The conductance is

$$S_D = \frac{3\pi a^4 \tau}{8M\bar{c}\ell L}$$

Compare the conductance of the tube in hydrodynamic limit with  $S_{hole} = \frac{1}{4} \bar{c} \cdot A$ . Making use of  $\bar{c}^2 = 8\tau/\pi M$ ,

$$S_D = S_{hole} \cdot \left( \frac{\pi a}{L} \right) \cdot \left( \frac{3a}{16\ell} \right)$$

$\uparrow$  small       $\uparrow$  large

Thus,  $S_D$  and  $S_{hole}$  can be of the same order.

But, we can also compare  $S_D$  and  $S_{tube}$

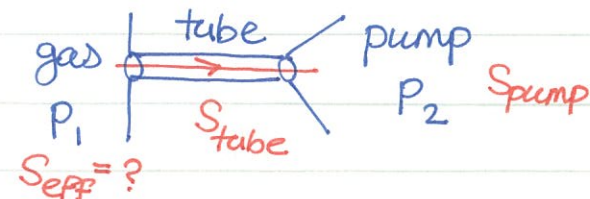
$$\frac{S_D}{S_{tube}} = \frac{3a}{16\ell} \gg 1$$

$\rightarrow S_D \gg S_{tube}$  The conductance of the same geometry is much larger in hydrodynamic regime!

① **Speed of a pump**: It is defined as the volume pumped per unit time at the intake pressure of the pump.

$$S_{\text{pump}} \equiv \frac{dV}{dt} = \frac{1}{n} \left( n \frac{dV}{dt} \right) = \frac{1}{n} \Phi$$

Similar to conductance defined before.

Consider the pumping setup:  For given conductance  $S_{\text{tube}}$  and pumping speed  $S_{\text{pump}}$ , we would like to know how fast the gas is pumped out... The flux is constant in the steady state,

$$\Phi = n_2 S_{\text{pump}} = (n_1 - n_2) S_{\text{tube}} = n_1 S_{\text{eff}}$$

Express  $S_{\text{eff}}$  in terms of  $S_{\text{pump}}$ ,  $S_{\text{tube}}$ .

$$\frac{S_{\text{eff}}}{S_{\text{pump}}} = \frac{n_2}{n_1} \quad \text{and} \quad \frac{S_{\text{eff}}}{S_{\text{tube}}} = \frac{n_1 - n_2}{n_1}$$

Adding these two identities together,

$$S_{\text{eff}} \left( \frac{1}{S_{\text{pump}}} + \frac{1}{S_{\text{tube}}} \right) = 1 \rightarrow \frac{1}{S_{\text{eff}}} = \frac{1}{S_{\text{pump}}} + \frac{1}{S_{\text{tube}}}$$

This is similar to the addition of resistance in series  $R_{\text{eff}} = R_1 + R_2$ . It is clear that  $S_{\text{eff}} < S_{\text{pump}}$ . Therefore, to make the pump efficient, a larger conductance  $S_{\text{tube}}$  is required ☺



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