



LAPLACE
TRANSFORM AND
ITS APPLICATION
IN CIRCUIT
ANALYSIS

C.T. Pan

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12.1 Definition of the Laplace Transform

Pierre Simon Laplace (1749-1827):

A French astronomer and mathematician *First* presented the Laplace transform and its applications to differential equations in 1979.

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12.1 Definition of the Laplace Transform

Definition:

$$L[f(t)] = F(s) = \int_{0^{-}}^{\infty} f(t)e^{-st}dt$$

$$s = s + jw \quad \text{a complex variable}$$

The Laplace transform is an integral transformation of a function f(t) from the time domain into the complex frequency domain, F(s).

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12.1 Definition of the Laplace Transform

One-sided (unilateral) Laplace transform Two-sided (bilateral) Laplace transform

$$L^{-1}[F(s)] = f(t) = \frac{1}{2p j} \int_{s_1 - jw}^{s_1 + jw} F(s)e^{st} ds$$

Look-up table, an easier way for circuit application $f(t) \Leftrightarrow F(s)$

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12.1 Definition of the Laplace Transform

Similar to the application of phasor transform to solve the steady state AC circuits, Laplace transform can be used to transform the time domain circuits into S domain circuits to simplify the solution of integral differential equations to the manipulation of a set of algebraic equations.

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12.2 Useful Laplace Transform Pairs

Functions	f(t), t>0	F(s)
impulse	d(t)	1
step	u(t)	$\frac{1}{S}$
ramp	t	$\frac{1}{S^2}$
exponential	e^{-at}	$\frac{1}{S+a}$
sine	sin wt	$\frac{w}{S^2 + w^2}$

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12.2 Useful Laplace Transform Pairs

Functions	f(t), t>0 ⁻	F(s)
cosine	cos Wt	$\frac{S}{S^2 + w^2}$
damped ramp	te^{-at}	$\frac{1}{\left(S+a\right)^2}$
damped sine	$e^{-at}\sin wt$	$\frac{w}{\left(S+a\right)^2+w^2}$
damped cosine	$e^{-at}\cos wt$	$\frac{S+a}{\left(S+a\right)^2+w^2}$

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12.2 Useful Laplace Transform Pairs

$$\Delta L \left[\frac{d}{dt} f(t) \right] = sF(s) - f(0^{-})$$

$$\Delta L \left[\int_{0^{+}}^{t} f(t) dt \right] = \frac{F(s)}{S}$$

$$\Delta L \left[f(t-a)u(t-a) \right] = e^{-as} F(s), a > 0$$

$$\Delta L \left[e^{-at} f(t) \right] = F(s+a)$$

$$\Delta L[f(at)] = \frac{1}{a}F(\frac{s}{a}), a > 0$$

$$\Delta \lim_{t \to 0^+} [f(t)] = \lim_{s \to \infty} sF(s)$$

$$\Delta \lim_{t \to \infty} [f(t)] = \lim_{s \to 0} sF(s)$$

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12.2 Useful Laplace Transform Pairs

Example Use the Laplace transform to solve the differential equation.

$$\frac{d^2v}{dt^2} + 6\frac{dv}{dt} + 8v = 2u(t)$$

$$v(0) = 1$$

$$v'(0) = -2$$

Take Laplace transfrom

$$[s^{2}V(s) - sv(0) - v'(0)] + 6[sV(s) - v(0)] + 8V(s) = \frac{2}{s}$$

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12.2 Useful Laplace Transform Pairs

$$\left[s^{2}V(s) - sv(0) - v'(0) \right] + 6 \left[sV(s) - v(0) \right] + 8V(s) = \frac{2}{s}$$

$$(s^{2} + 6s + 8)V(s) = \frac{s^{2} + 4s + 2}{s}$$

$$\therefore V(s) = \frac{s^{2} + 4s + 2}{s(s^{2} + 6s + 8)} = \frac{s^{2} + 4s + 2}{s(s + 2)(s + 4)}$$

$$v(t) = \frac{1}{4} (1 + 2e^{-2t} + e^{-4t})u(t)$$

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(1) KCL, $\sum_{n} i_k(t) = 0$, for any node.

Take Laplace Transform

$$\sum_{n} I_k(s) = 0$$
, for any node.

(2) KVL, $\sum_{m} v_k(t) = 0$, for any loop.

Take Laplace Transform

$$\sum_{m} V_k(s) = 0 , \text{ for any loop.}$$

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12.3 Circuit Analysis in S Domain

(3) Circuit Component Models resistor

$$v_R(t) = Ri_R(t)$$
$$V_R(s) = RI_R(s)$$

$$I_R(s) = GV_R(s)$$

 $\begin{array}{c}
I_R(s) \\
+ \\
V_R(s) & R \\
- \\
\end{array}$

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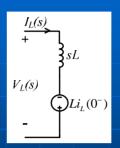
inductor

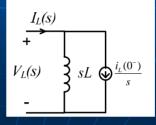
$$v_L(t) = L \frac{di_L}{dt}$$

$$i_L(t) = i_L(0^-) + \frac{1}{L} \int_{0^-}^t v_L(t) dt$$

$$V_L(s) = sLI_L(s) - Li_L(0^-)$$

$$I(s) = \frac{V_L(s)}{sL} + \frac{i_L(0^-)}{s}$$





12.3 Circuit Analysis in S Domain

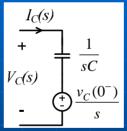
capacitor

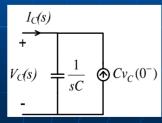
$$i_C = C \frac{dv_C}{dt}$$

$$dt v_C(t) = v_C(0^-) + \frac{1}{C} \int_{0^-}^{t} i_C(t) dt$$

$$I_C(s) = sCV_C(s) - Cv_c(0^-)$$

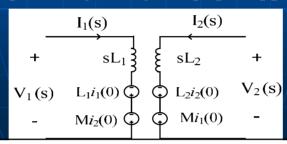
$$V_C(s) = \frac{v_C(0^-)}{s} + \frac{1}{sC}I_C(s)$$





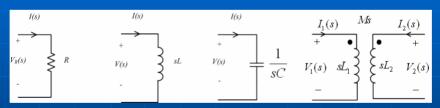
Coupling inductors

 $\begin{aligned} & V_1(s) = & L_1 S I_1(s) - L_1 i_1(0) + M S I_2(s) - M i_2(0) \\ & V_2(s) = & M S I_1(s) - M i_1(0) + L_2 S I_2(s) - L_2 i_2(0) \end{aligned}$



12.3 Circuit Analysis in S Domain

For zero initial conditions



impedance @
$$\frac{V(s)}{I(S)} = Z(s)$$

admittance @
$$\frac{I(S)}{V(s)} = Y(s) = \frac{1}{Z(s)}$$

V(s) = Z(s)I(s) ohm's law in s – domain

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The elegance of using the Laplace transform in circuit analysis lies in the automatic inclusion of the initial conditions in the transformation process, thus providing a complete (transient and steady state) solution.

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12.3 Circuit Analysis in S Domain

Circuit analysis in s domain

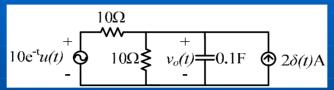
nStep 1 : Transform the time domain circuit into s-domain circuit.

nStep 2 : Solve the s-domain circuit. e.g. Nodal analysis or mesh analysis.

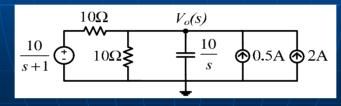
nStep 3 : Transform the solution back into time domain.

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Example Find $v_o(t)$ given $v_o(0)=5V$



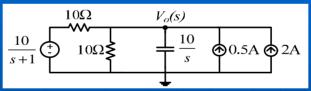
S-domain equivalent circuit



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12.3 Circuit Analysis in S Domain



Nodal analysis

$$\frac{\frac{10}{s+1} - V_o(s)}{10} + 2 + 0.5 = \frac{V_o(s)}{10} + \frac{V_o(s)}{10/s}$$

$$\therefore V_o(s) = \frac{25s + 35}{(s+1)(s+2)} = \frac{10}{s+1} + \frac{15}{s+2}$$

$$\therefore v_o(t) = (10e^{-t} + 15e^{-2t})u(t) \text{ V}$$

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2:

Given a linear circuit N in s domain as shown below

input X(s) output Y(s)

Transfer function H(s) is defined as

$$H(s) = \frac{Y(s)}{X(s)} \Big|_{\text{With zero initial condition}}$$

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12.4 The Transfer Function and the Convolution Integral

If $Y(s) = V_o(s)$, $X(s) = V_i(s)$; then H(s) = voltage gain

If $Y(s) = I_o(s)$, $X(s) = I_i(s)$; then H(s) = current gain

If Y(s) = V(s), X(s) = I(s); then H(s) = impedance

If Y(s) = I(s), X(s) = V(s); then H(s) = admittance

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Given the transfer funtion H(s) and input X(s), then Y(s)=H(s)X(s)

If the input is δ (t), then X(s)=1 and Y(s)=H(s)

Hence, the physical meaning of H(s) is in fact the Laplace transform of the impulse response of the corresponding circuit.

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12.4 The Transfer Function and the Convolution Integral

Y(s)=H(s)X(s), in s-domain

$$y(t) = \int_{-\infty}^{\infty} h(t-t)x(t)dt @ h(t) * x(t)$$
 in time domain

Geometrical interpretation of finding the convolution integral value at $t=t_k$ is based on :

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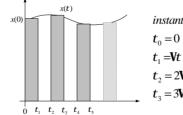
- (1)Approximating the input function by using a series of impulse functions.
- (2)Shifting property of linear systems input x(t)—output y(t) $x(t-\tau)$ —output $y(t-\tau)$
- (3)Superposition theorem for linear systems
- (4)Definition of integral: finding the area

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12.4 The Transfer Function and the Convolution Integral

(1)Input x(τ) is approximated using impulse functions, x(τ)=0, for τ <0



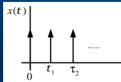
instant \mathbf{t}_{k} , $\mathbf{x}(\mathbf{t}_{k})$ value, area

 $t_0 = 0$, x(0) , x(0)**V**t

 $t_1 = Vt$, $x(t_1)$, $x(t_1)Vt$

 $t_2 = 2\mathbf{V}t \quad , \quad x(t_2) \qquad , x(t_2)\mathbf{V}t$

 $t_3 = 3\mathbf{V}t \quad , \quad x(t_3) \qquad , x(t_3)\mathbf{V}t$



 $x(t) \cong f_0 d(t) + f_1 d(t - t_1) + f_2 d(t - t_2) + \mathbf{L}$

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(2) Use the linearity property

$$\begin{array}{ccc} input & \longrightarrow & output(response) \\ x(0) \mathbf{V}td(t) & \longrightarrow & x(0) \mathbf{V}th(t) \\ x(t_1) \mathbf{V}td(t-t_1) & \longrightarrow & x(t_1) \mathbf{V}th(t-t_1) \\ x(t_2) \mathbf{V}td(t-t_2) & \longrightarrow & x(t_2) \mathbf{V}th(t-t_2) \\ & \mathbf{M} & \mathbf{M} \\ up \ to \ t = t_k \end{array}$$

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12.4 The Transfer Function and the Convolution Integral

(3) Use superposition theorem to find the total approximate response

$$\mathbf{\hat{y}}(t_k) = \sum_{k=0}^{n} x(k\mathbf{V}t)\mathbf{V}t \ h(t_k - k\mathbf{V}t)$$

$$n = integer[\frac{t_k}{\mathbf{V}t}]$$

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(4) Take the limit, $\Delta \tau \rightarrow d \tau$, $(t_k) \longrightarrow y(t_k)$

$$y(t_k) = \int_{-\infty}^{\infty} x(t)h(t_k - t)dt$$

Due to causality principle, $h(t-\tau)=0$ for $t \ge t_k$ and x(τ)=0 for τ <0

$$=\int_{0}^{t_{k}}h(t_{k}-t)x(t)dt$$

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12.4 The Transfer Function and the **Convolution Integral**

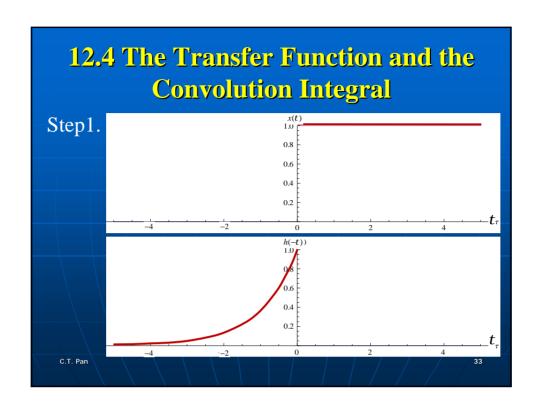
Example:

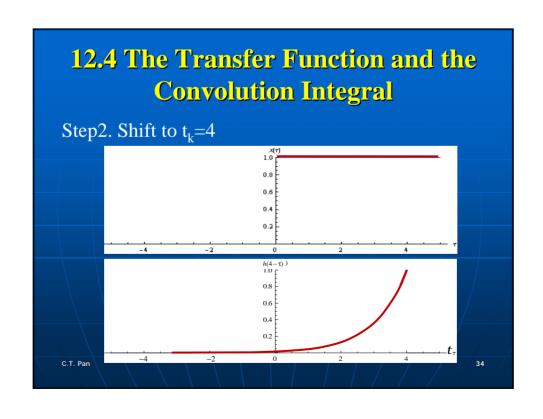
Given
$$x(t) = u(t)$$
, $h(t) = e^{-t}u(t)$, find $y(4)$,

$$y(t) = \int_{-\infty}^{\infty} h(t-t)x(t)dt$$
$$\therefore y(4) = \int_{-\infty}^{\infty} h(4-t)x(t)dt$$

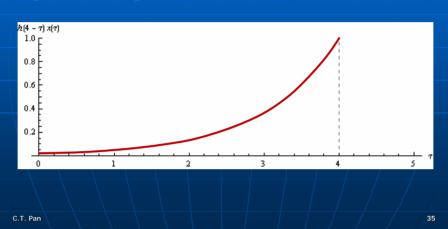
$$\therefore y(4) = \int_{-\infty}^{\infty} h(4-t)x(t)dt$$

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Step3. Find the product h(4- τ)x(τ)



12.4 The Transfer Function and the Convolution Integral

Step4. Find the integral (area)

$$y(4) = \int_0^4 e^{-(4-t)} dt = e^{-4} \int_0^4 e^t dt = e^{-4} e^t \Big|_0^4$$
$$= e^{-4} (e^4 - 1) = (1 - e^{-4})$$

 $\therefore y(4) = (1 - e^{-4})$

Step5. Check

$$Y(s) = H(s)X(s) = \frac{1}{s+a} \times \frac{1}{s} = \frac{-\frac{1}{a}}{s+a} + \frac{1}{a}$$

$$\therefore y(t) = \frac{1}{a}(1-e^{-t}), a=1$$

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From definition of transfer function

$$H(s) = \frac{Y(s)}{X(s)}$$

$$\Rightarrow Y(s) = H(s)X(s)$$

Assume input $X(t)=A\cos(wt+\Phi)$ and H(s) is given, then one can get the steady state solution without needing a separate phasor analysis.

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12.5 The Transfer Function and the Steady State Sinusoidal Response

$$proof: X(t) = A\cos f\cos \omega t - A\sin f\sin \omega t$$

$$\therefore X(s) = \frac{A(\cos f s - \sin f \omega)}{s^2 + \omega^2}$$

$$\therefore Y(s) = H(s)X(s)$$

$$=\frac{K_1}{s-j\omega}+\frac{{K_1^*}}{s+j\omega}$$

 $+\sum$ other terms due to poles

under steady state:

$$\therefore Y_{ss}(s) = \frac{K_1}{s - j\omega} + \frac{K_1^*}{s + j\omega}$$

$$K_{1} = \frac{H(s)A(s\cos f - \omega\sin f)}{s + j\omega}\bigg|_{s = j\omega}$$

$$=\frac{1}{2}H(j\omega)Ae^{jf}$$

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Let
$$H(j\omega) = |H(j\omega)| e^{jq(\omega)}$$

and take inverse Laplace transform

Then
$$y_{ss}(t) = A | H(j\omega) | \cos[\omega t + f + q(\omega)]$$

i.e.
$$P(X(t)) = A \angle f$$

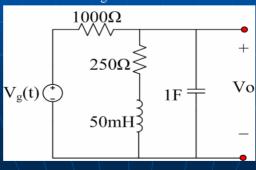
then
$$P(y_{ss}(t)) = A | H(j\omega) | \angle f + q(\omega)$$

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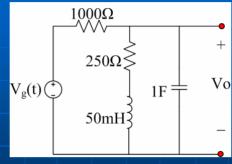
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12.5 The Transfer Function and the Steady State Sinusoidal Response

the given $V_g(t)$.



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$$H(s) = \frac{1000(s+5000)}{s^2 + 6000s + 25 \cdot 10^6}$$
$$V_g(t) = 120\cos(5000t + 30^\circ) V$$

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12.5 The Transfer Function and the Steady State Sinusoidal Response

Solution: Let
$$s = j\omega = j5000$$

Evaluate
$$H(j5000) = \frac{1000(j5000 + 5000)}{-25 \times 10^6 + j5000(6000) + 25 \times 10^6}$$

= $\frac{\sqrt{2}}{6} \angle -45^\circ$

Then
$$V_o^{ss}(t) = 120 \times \frac{\sqrt{2}}{6} \cos(5000t + 30^\circ - 45^\circ)$$

= $20\sqrt{2} \cos(5000t - 15^\circ) V$

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nIn theory, the relationship between H(s) and H(jw) provides a link between the time domain and the frequency domain.

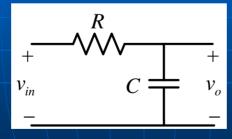
nIn some cases, we can determine H(jw) experimentally and then construct H(s) from the data.

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12.5 The Transfer Function and the Steady State Sinusoidal Response

Example: Find the impulse response of the following circuit.



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(a) Time domain solution

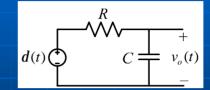
$$RC\frac{dv_{o}}{dt} + v_{o} = d(t)$$

$$At \ t = 0^{-}, \ v_{o}(0^{-}) = 0$$

$$At \ t = 0^{+}, \ v_{o}(0^{+}) = \frac{1}{C} \int_{0}^{t} \frac{d(t)}{R} dt$$

$$C \int_{0}^{\infty} R dt$$

$$= \frac{1}{RC} V$$



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12.5 The Transfer Function and the Steady State Sinusoidal Response

For $t > 0^+$, d(t) = 0

$$C \xrightarrow{+} v_o(t) , v(0^+) = \frac{1}{RC}$$

$$RC\frac{dv_o}{dt} + v_o = 0$$

$$\therefore v_o(t) = \frac{1}{RC}e^{-\frac{t}{RC}}u(t)$$

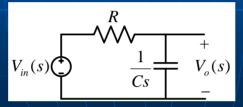
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(b) s-domain solution

Find the transfer function

$$H(s) = \frac{V_o(s)}{V_{in}(s)}\bigg|_{zero\ I.C.}$$

Transform into s-domain circuit



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12.5 The Transfer Function and the Steady State Sinusoidal Response

$$\therefore H(s) = \frac{V_o(s)}{V_{in}(s)} = \frac{\frac{1}{Cs}}{R + \frac{1}{Cs}} = \frac{1}{1 + RCs}$$

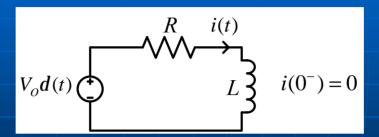
$$\therefore h(t) = L^{-1}[H(s)]$$
$$= \frac{1}{RC}e^{-\frac{t}{RC}}u(t)$$

 $V_{in}(s)$ $\begin{array}{c|c}
 & R \\
\hline
 & 1 \\
\hline
 & Cs \\
\hline
 & - \\
\end{array}$

Same answer.

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Example 1: Impulse voltage source excitation



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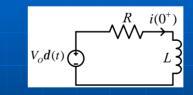
12.6 The Impulse Function in Circuit Analysis

(a) Time domain solution

$$At t = 0, i(0^{-}) = 0$$

$$\therefore i(0^{+}) = \frac{1}{L} \int_{0^{-}}^{t} V_{O} d(x) dx$$

$$= \frac{V_{O}}{L} (A)$$



The impulse voltage source has stored energy, $\frac{1}{2}L(i(0^{\circ}))^2$, in the inductor as an initial current in an infinitesimal moment.

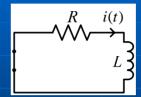
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For $t > 0^+$, d(t) = 0

$$L\frac{di}{dt} + Ri = 0$$
, natural response

$$i(0^+) = \frac{V_O}{L} A$$

$$\therefore i(t) = \frac{V_O}{L} e^{-t/t} u(t) , \quad t = \frac{L}{R}$$



Note that the impulse source just builds up an initial inductor current but does not contribute to any forced response.

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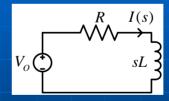
12.6 The Impulse Function in Circuit **Analysis**

(b) s-domain solution

$$\therefore I(s) = \frac{V_O}{R + sL} = \frac{V_O / L}{s + \frac{R}{L}}$$

$$\therefore i(t) = \frac{V_O}{L} e^{-t/t} u(t)$$

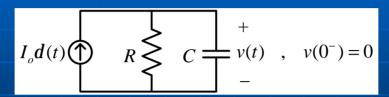
$$\therefore i(t) = \frac{V_O}{I} e^{-t/t} u(t)$$



Same answer but much easier.

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Example 2: Impulse current source excitation



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12.6 The Impulse Function in Circuit Analysis

(a) Time domain solution

$$At \ t = 0, \ v(0^-) = 0$$

$$v(0) = 0$$
, short circuit

$$I_o d(t)$$
 $R \ge 1$

$$v(0^+) = \frac{1}{C} \int_0^t I_o d(x) dx$$
$$= \frac{I_o}{C}$$

The impulse current source has stored energy, $\frac{1}{2}C(v(0^{\circ}))^2$, in the capacitor as an initial voltage in an infinitesimal moment.

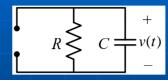
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For $t > 0^+$, d(t) = 0, open circuit

$$C\frac{dv}{dt} + \frac{v}{R} = 0$$
, natural response

$$v(0^+) = \frac{I_o}{C}$$

$$\therefore v(t) = \frac{I_o}{C} e^{-\frac{t}{t}} u(t) , t = RC$$



Note that the impulse current just builds up an initial capacitor voltage but does not contribute to any forced response.

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12.6 The Impulse Function in Circuit Analysis

(b) s-domain solution

Transform into s-domain circuit

$$I_o \bigoplus R \gtrless C \Longrightarrow V(s)$$

$$\therefore V(s) = I_o \frac{R \times \frac{1}{Cs}}{R + \frac{1}{Cs}} = \frac{I_o / C}{s + \frac{1}{RC}}$$

$$\therefore v(t) = \frac{I_o}{C} e^{-\frac{t}{t}} u(t)$$

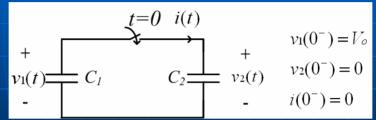
Same answer but much easier.

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Example 3: Impulse caused by switching operation

The switch is closed at t=0 in the following circuit.



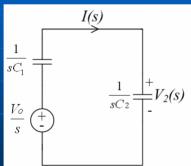
Note that $v_1(0^-) \neq v_2(0^-)$

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12.6 The Impulse Function in Circuit Analysis

Transform into s-domain



$$I(s) = \frac{\frac{V_o}{s}}{\frac{1}{sC_1} + \frac{1}{sC_2}} @V_o \cdot C_e$$

$$\frac{1}{sC_2} = \frac{V_o \cdot C_e}{\frac{1}{sC_1} + \frac{1}{sC_2}} @V_o \cdot C_e$$

$$C_e = \frac{C_1 \cdot C_2}{C_1 + C_2}, V_2(s) = \frac{V_o \cdot C_e}{sC_2} = \frac{V_o}{s} \cdot \frac{C_1}{C_1 + C_2}$$

$$\therefore i(t) = V_o C_e d(t)$$

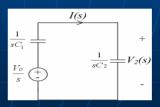
$$v_2(t) = \frac{C_1}{C_1 + C_2} V_o$$

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At t=0, a finite charge of C_1 is transferred to C_2 instantaneously.

Note that , as the switch is closed , the voltage across C_2 does not jump to $V_{\scriptscriptstyle 0}$ of C_1 but to its final value of the two paralleled capacitors.



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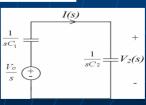
12.6 The Impulse Function in Circuit Analysis

Note
$$Q_2 = C_2 \cdot V_2 = \frac{C_1 \cdot C_2}{C_1 + C_2} V_o, t > 0^+$$

$$Q_1 = C_1 \cdot V_2 = \frac{C_1^2}{C_1 + C_2} V_o, t > 0^+$$

$$Q_1 + Q_2 = C_1 V_o, t > 0^+$$
Also, at $t = 0^-$, $Q_1 = C_1 V_o$, $Q_2 = 0$

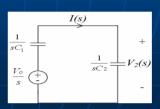
$$\therefore Q_1 + Q_2 = C_1 V_o$$
Conservation of charge.



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If we consider charged capacitors as voltage sources, then we should not connect two capacitors with unequal voltages in parallel.

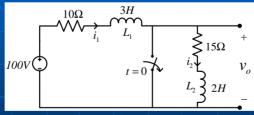
Due to violation of KVL, an impulse will occur which may damage the components.



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12.6 The Impulse Function in Circuit Analysis

Example 4: Impulse caused by switching operation The switch is opened at t = 0 in the following circuit.



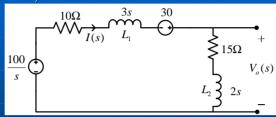
At $t = 0^-$, steady state solution

$$i_1(0^-) = \frac{100V}{10\Omega} = 10 A$$

$$i_2(0^-) = 0 A$$

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For t > 0, the S-domain circuit is



$$I(s) = \frac{(100/s) + 30}{5s + 25} = \frac{4}{s} + \frac{2}{s + 5}$$

$$V_o(s) = I(s) (2s + 15) = 12 + \frac{60}{s} + \frac{10}{s + 5}$$

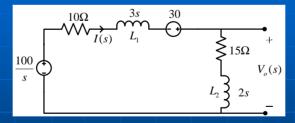
$$\therefore i(t) = (4 + 2e^{-5t}) u(t) \dots (A)$$

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 $v(t) = 12d(t) + (60 + 10e^{-5t}) u(t) \dots (B)$

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12.6 The Impulse Function in Circuit Analysis

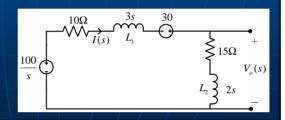


Note
$$t = 0$$
, $i_{L1}(0^{-}) = 10 A$, $i_{L2}(0^{-}) = 0 A$
 $t = 0^{+}$, from (A), $i_{L1}(0^{+}) = 6 A$, $i_{L2}(0^{+}) = 6 A$
Also, from (B), there exists $12d(t)$ at $v_o(t)$.

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Thus, if we consider an inductor current as a current source, then two inductors with unequal currents should not be connected in series.

Due to violation of KCL, it will result in impulse voltage which may damage the components.



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SUMMARY

Objective 1 : Know the component models in s-domain.

Objective 2 : Be able to transform a time domain circuit into the s-domain circuit.

Objective 3: Know how to analyze the s-domain circuit and transform the solution back to time domain.

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SUMMARY

Objective 4 : Understand the significance of transfer function and be able to calculate the transfer function from the s-domain circuit.

Objective 5 : Know the geometrical interpretation of convolution integral and be able to calculate the integral.

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SUMMARY

Objective 6: Know the relation between the phasor solution technique for finding sinusoidal steady state solution and the s-domain solution technique.

Objective 7: Know how to use s-domain solution technique to solve a circuit containing impulse sources or a switching circuit which may result in impulse functions.

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SUMMARY				
Chapter problem	ıs:			
	13.13			
	13.20			
	13.27			
	13.36			
	13.57			
	13.85			
	13.88			
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